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PISCATAQUA RIVER BAŞIN ROLLINSFORD, NEW HAMPSHIRE

ROLLINSFORD DAM NH 00396

STATE NO 205.02

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM





DEPARTMENT OF THE ARMY
NEW ENGLAND DIVISION, CORPS OF ENGINEERS
WALTHAM, MASS. 02154

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DECEMBER 1979

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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

DAMS, INSPECTION, DAM SAFETY,

Piscataqua River Basin Rollinford New Hampshire Salmon Falls River

20. ABSTRACT (Cantinue on reverse side if necessary and identify by block number)

The dam is a run of the rive split stone and concrete gravity da. It is 385 ft. long adn 20 ft. high. The dam is in fair condition with a few major concerns which must be corrected. It is small in size with a significant hazard potential.

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DEPARTMENT OF THE ARMY

NEW ENGLAND DIVISION, CORPS OF ENGINEERS

424 TRAPELO ROAD

WALTHAM, MASSACHUSETTS 02154

REPLY TO ATTENTION OF NEDED

APR 2.3 1990

Honorable Hugh J. Gallen Governor of the State of New Hampshire State House Concord, New Hampshire 03301

Dear Governor Gallen:

Inclosed is a copy of the Rollinsford Dam Phase I Inspection Report, which was prepared under the National Program for Inspection of Non-Federal Dams. This report is presented for your use and is based upon a visual inspection, a review of the past performance and a brief hydrological study of the dam. A brief assessment is included at the beginning of the report. I have approved the report and support the findings and recommendations described in Section 7 and ask that you keep me informed of the actions taken to implement them. This follow-up action is a vitally important part of this program.

A copy of this report has been forwarded to the Water Resources Board, the cooperating agency for the State of New Hampshire. In addition, a copy of the report has also been furnished the owner, the town of Rollinsford.

Copies of this report will be made available to the public, upon request, by this office under the Freedom of Information Act. In the case of this report the release date will be thirty days from the date of this letter.

I wish to take this opportunity to thank you and the Water Resources Board for your cooperation in carrying out this program.

Sincerely,

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NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT

Identification No.: NH00396

Name of Dam: Rollinsford Dam
Town: Rollinsford

County and State: Strafford County, New Hampshire

River: Salmon Falls River
Date of Inspection: October 25, 1979

BRIEF ASSESSMENT

Rollinsford Dam is a run-of-the-river split-stone and concrete gravity dam. The dam totals 385 feet in length and has a hydraulic height of 20 feet. The northeast abutment consists of a stone masonry wall. At the southwest abutment are remnants of an approach channel, gates, and penstock structure. The approach channel and gate area have been filled with earth and the gate operators have been removed. The dam is located on the eastern boundary of the State of New Hampshire. The dam impounds a reservoir with a maximum storage capacity of 820 acrefeet. The reservoir is 0.9 miles in length with a surface area of 57 acres. The impoundment behind the dam is utilized as one of the main sources of water for fire protection for the Town of Rolinsford.

The dam is in fair condition. Concerns are the major seepage at the base of the dry stone masonry training wall at the southwest end of the spillway; erosion of the ground between the northeast end of the dam and the railroad pier; possible subsidence of earthfill next to the southwest end of the dam; and no usable low-level outlet.

Based on small size and significant hazard classification in accordance with Corps guidelines, the test flood ranges from the 100-year to by the Probable Maximum Flood (PMF). Because the dam's size is in the upper range of the size classification, & PMF was selected as the test flood. The watershed consists of 230 square miles of gently to moderately sloping partly wooded terrain. The test flood inflow was determined to be 34,500 cfs. Routing through the reservoir resulted in negligible surcharge storage effects in reducing the peak Therefore the routed test flood outflow equals the peak inflow value of 34,500 cfs (150 csm) at elevation 82' NGVD. test flood analysis indicates the dam would be overtopped by about 7.4 feet (12 feet over spillway crest) during the test flood conditions. Spillway capacity at top of dam is 7,010 cfs which is 20 percent of the test flood discharge. A major breach of the dam would probably not result in any loss of life but could cause appreciable property damage.

The owner, Town of Rollinsford, should implement the results of the recommendations and remedial measures given in Sections 7.2 and 7.3 within one year after receipt of this Phase I Apspection Report.

Warren A. Guinan Project Manager N.H. P.E. 2339

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This Phase I Inspection Report on Rollinsford Dam has been reviewed by the undersigned Review Board members. In our opinion, the reported findings, conclusions, and recommendations are consistent with the Recommended Guidelines for Safety Inspection of Dams, and with good engineering judgment and practice, and is hereby submitted for approval.

Chromat Waterin

ARAMAST MAHTESIAN, MEMBER Geotechnical Engineering Branch Engineering Division

Carney M. Tazion

CARNEY M. TERZIAN, MEMBER Design Branch Engineering Division

RICHARD DIBUONO, CHAIRMAN

Water Control Branch

Engineering Division

APPROVAL RECOMMENDED:

OE B. FRYAR

Chief, Engineering Division

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

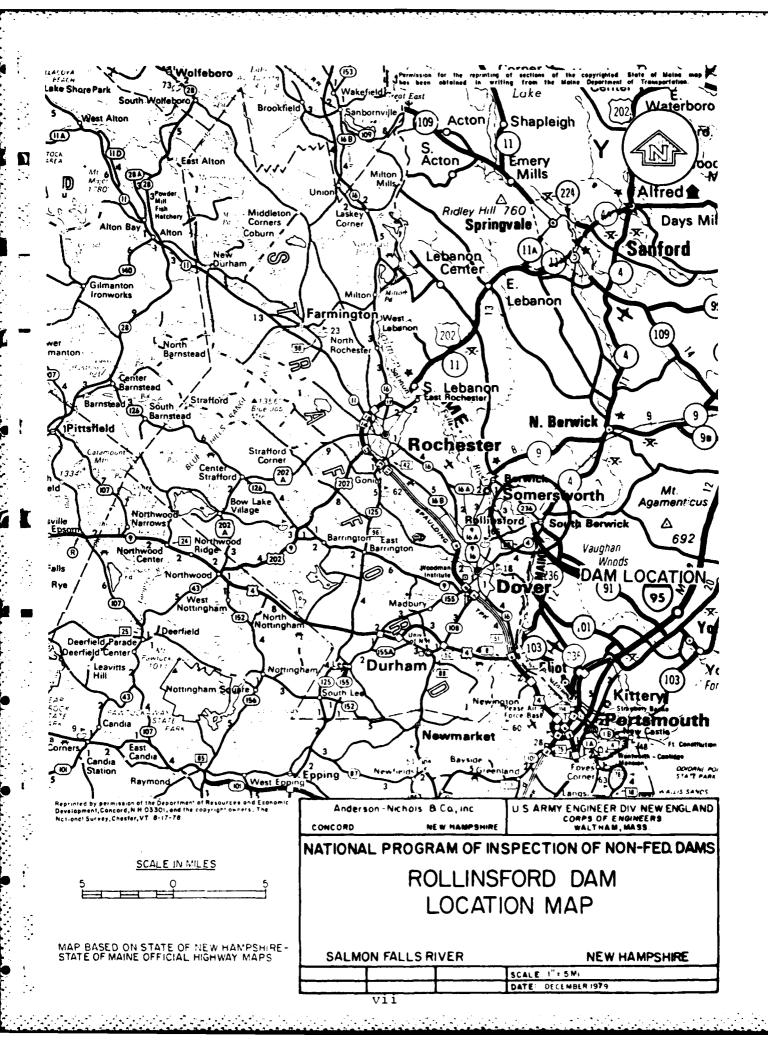
Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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October 1979 Figure 1 - Overview of Rollinsford Dam.



NATIONAL DAM INSPECTION PROGRAM PHASE I INSPECTION REPORT ROLLINSFORD DAM

SECTION 1 PROJECT INFORMATION

1.1 General

a. Authority. Public Law 92-367, August 8, 1972 authorized the Secretary of the Army, through the Corps of Engineers, to ritiate a National Program of Dam Inspection throughout the 'nited States. The New England Division of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the New England Region. Anderson-Nichols & Company, Inc. has been retained by the New England Division to inspect and report on selected dams in the State of New Hampshire. Authorization and notice to proceed were issued to Anderson-Nichols under a letter of March 22, 1979 from John P. Chandler, Corps of Engineers. Contract No. DACW33-79-C-0050, as changed, has been assigned by the Corps of Engineers for this work.

b. Purpose

- (1) To perform technical inspection and evaluation of non-Federal dams to identify conditions which threaten the public safety and thus permit correction in a timely manner by non-Federal interests.
- (2) To encourage and prepare the States to initiate quickly effective dam safety programs for non-Federal dams.
- (3) To update, verify and complete the National Inventory of Dams.

1.2 Description of Project

a. Location. Rollinsford Dam, commonly known as Salmon Falls River Dam #2, is located in the Towns of Rollinsford, New Hampshire and Berwick, Maine. The dam is a run-of-the-river dam spanning Salmon Falls River approximately 5 miles above its confluence with the Cocheco River. The centerline of the river serves as the boundary between New Hampshire and Maine. The Piscataqua River originates at the confluence of the Salmon Falls and Cocheco Rivers. Rollinsford Dam is shown on USGS 7.5-Minute Quadrangle, Dover East, Maine - New Hampshire and 15-Minute Quadrangle, Dover, New Hampshire - Maine with coordinates approximately at N 43° 14' 17", W 70° 49' 06". Rollinsford is located in Strafford County, New Hampshire and Berwick is located in York County, Maine. (See Location Map, page vii.)

- b. Description of Dam and Appurtenances. Rollinsford Dam is a run-of-the-river dam totaling 385 feet in length and having a hydraulic height of 20 feet. The dam is a split-stone and concrete gravity dam. The northeast spillway abutment consists of a stone masonry wall. An earth fill section exists between this abutment 70 feet to a railroad pier. The concrete gravity spillway is 245 feet long and has a sloping downstream face. At the southwest abutment are remnants of an approach channel, gates, and penstock structure. The approach channel and gate area have been filled with earth and the gate operators have been removed. An access road runs perpendicular to the southwest abutment of the dam.
- c. Size Classification. Small (hydraulic height 20 feet; storage 820 acre-feet) based on storage (≥ 50 to < 1000 acrefeet) as given in Recommended Guidelines for Safety Inspection of Dams.
- d. Hazard Classification. Significant Hazard. A major breach would probably result in no loss of life but could cause appreciable property damage. The pondage behind this dam is utilized as one of the main sources of water for fire protection for the Town of Rollinsford. Therefore, loss of pondage would result in interruption of the services of a public utility. In addition damage to the railroad bridge piers could occur. (See 5.1 f.)
- e. Ownership. No records were found which revealed the original owners of the dam. In 1935, the Public Service Company of New Hampshire is reported to have had ownership. According to found records, the Twin State Gas and Electric Company owned the structure in 1940. In 1950 ownership is again listed as Public Service Company of New Hampshire. Ownership was conveyed to the Town of Rollinsford sometime in 1973. The Town of Rollinsford has since remained the owner of the dam.
- f. Operator. The current owner and operator of the Rollinsford Dam is the Town of Rollinsford, Rollinsford, New Hampshire.
- g. Purpose of Dam. The purpose of the original construction is believed to have been for water power production for the mill complex downstream. The dam was utilized for hydropower generation for both the Public Service Company and the Twin State Gas and Electric Company. Presently, the pondage behind the dam supplies one of the two main sources of water for fire protection for the Town of Rollinsford.
- h. Design and Construction History. No information was found regarding the design or construction of the dam. The dam appears to be of the vintage of the mid 1800's. The southwest end of the dam did contain power generating facilities. The intake channel and headgates to the powerhouse were filled in sometime prior to 1970.

i. Normal Operating Procedures. The dam currently acts only as a river barrier with its pondage providing water for the Rollinsford Fire Department.

1.3 Pertinent Data

a. Drainage Area. The drainage area consists of 230 square miles (147,200 acres) of gently to moderately sloping partly wooded terrain. The normal pool has a surface area of 57 acres, which constitutes 0.04 percent of the watershed.

b. Discharge at Damsite

- (1) Outlet works (conduits): None at the present time.
- (2) The maximum discharge at damsite is unknown. No records of past overtoppings were disclosed.
- (3) Ungated spillway capacity @ top of dam elevation 7,010 cfs at 74.6' NGVD
- (4) Ungated spillway capacity @ test flood elevation -29,530 cfs at 82' NGVD
- (5) Gated spillway capacity at top of dam elevation not applicable
- (6) Gated spillway capacity at test flood elevation not applicable
- (7) Total spillway capacity at test flood elevation 29,530 cfs at 82' NGVD
- (8) Total project discharge at test flood elevation 34,500 cfs at 82' NGVD
- c. Elevation (ft. above NGVD of 1929; formerly Mean Sea Level (MSL), see (6) below.)
- (1) Streambed at centerline of dam 55 (at downstream toe)
 - (2) Maximum tailwater unknown
- (3) Upstream portal invert diversion tunnel not applicable
 - (4) Recreation pool not applicable
 - (5) Full flood control pool not applicable
- (6) Spillway crest 70.0 (obtained from USGS Quadrangle sheet and assumed to be spillway elevation)

- (7) Design surcharge (original design) unknown
- (8) Top dam 74.6
- (9) Test flood pool 82.0

d. Reservoir (miles)

- (1) Length of maximum pool 1
- (2) Length of spillway crest 0.9
- (3) Length of flood control pool not applicable

e. Storage (acre-feet)

- (1) Recreation pool not applicable
- (2) Flood control pool not applicable
- (3) Spillway crest pool 456
- (4) Test flood pool 1525
- (5) Top dam 820

f. Reservoir Surface (acres)

- (1) Recreation pool not applicable
- (2) Flood control pool not applicable
- (3) Spillway crest 57
- (4) Test flood pool 113
- (5) Top of dam 80

g. Dam

- (1) Type split-stone and concrete gravity dam
- (2) Length 385'
- (3) Height 23.5' structural height
- (4) Top width varies
- (5) Side slopes spillway upstream vertical; downstream sloping; abutments vertical upstream and downstream.
 - (6) Zoning unknown
 - (7) Impervious core unknown
 - (8) Cutoff unknown

- (9) Grout curtain unknown
- h. <u>Diversion and Regulating Tunnel</u> not applicable (See j. below)

i. Spillway

- (1) Type overflow spillway
- (2) Length of weir 245'
- (3) Crest elevation 70.0' NGVD
- (4) Gates none
- (5) U/S Channel Salmon Falls River. The banks are tree-lined.
- (6) D/S Channel Salmon Falls River. Discharge from dam flows southerly. A railroad bridge is located immediately downstream of the dam. Bedrock is exposed along most of the length of the dam. A road crossing is located 300 feet downstream of the dam. Salmon Falls River Dam is located 5500 feet downstream of Rollingsford Dam.
- j. Regulating Outlets. None operable; all gates and openings have been filled with earth.

SECTION 2 ENGINEERING DATA

2.1 Design

No design data were obtained for Rollinsford Dam.

2.2 Construction Records

No construction records were disclosed.

2.3 Operation

No engineering operational data were found.

2.4 Evaluation

- a. Availability. A search of the files of the New Hampshire Water Resources Board revealed only a limited amount of recorded information.
- b. Adequacy. Because of the limited amount of detailed data available the final assessments and recommendations of this investigation are based on the visual inspection and the hydrologic and hydraulic calculations.
 - c. Validity. No engineering data were found to validate.

SECTION 3 VISUAL INSPECTION

3.1 Findings

- a. General. Rollinsford Dam is a low dam which impounds a reservoir of small size. The watershed above the reservoir is gently to moderately sloping and partially wooded. The downstream area is flat to moderately sloping.
- b. <u>Dam</u>. Rollinsford Dam is a run-of-the-river split-stone and concrete gravity dam, with a hydraulic height of 20 feet and totaling 385 feet in length. (See Appendix C Figure 2.) Bedrock is exposed across the entire width of the river channel downstream of the dam and this observation is consistent with a statement in an undated data sheet of the New Hampshire Water Control Commission that the dam is founded on "ledge." (See Appendix C Figure 3.)

Remnants of an approach canal, head gates, and penstock entrance structure are located at the southwest abutment. The approach canal and gate area have been filled with earth and the gate operators have been removed. (See Appendix C - Figure 4.) Also, remnants of a large sluice gate are located just west of the former head gates. (See Appendix C - Figure 5.)

Major leakage is discharging at three locations at the base of the dry stone-masonry training wall at the southwest end of the overflow section of the dam. (See Appendix C - Figure 6.) The remnants of the gate structures are located between this wall and the southwest abutment. This is apparently the same leakage that was noted in the reports of inspections made on 11/30/77, 9/10/73, 6/30/50, and 7/14/40. Along the southwest abutment, just upstream of the dam, are the two pipes which the Rollinsford Fire Department uses to pump water from the impoundment behind the dam. (See Appendix C - Figure 7.)

The northeast abutment of the dam consists of a stone masonry wall. (See Appendix C - Figure 8.) At the northeast end of the dam it appears that flowing water has eroded a channel in the ground between the abutment block at the northeast end of the overflow section of the dam and a railroad pier which is about 75 feet from the end of the dam. (See Appendix C - Figure 9.)

c. Appurtenant Structures.

(1) The earth fill in the former approach channel at the southwest abutment is approximately 18 inches lower than the surrounding granite masonry walls at the gate structure. It could not be determined from the inspection whether this fill

has subsided or was originally placed in that manner. The existing intake structures have been blocked with earth fill, thus making it impossible to inspect. The downstream face of a small abandoned overflow structure, located at the right abutment approximately 30 feet downstream of the principal spillway, was severely eroded and the exposed wooden gate stems are badly weathered.

- (2) Principal spillway Only a limited portion of the spillway at each end could be inspected because of the flow of water over the dam. The surface of the concrete was observed to have minor surface erosion with some of the coarse aggregate exposed. No flashboards were on the spillway crest.
- d. Reservoir. The watershed above the reservoir is gently to moderately sloping and partially wooded. (See Appendix C Figure 10.) No evidence of significant sedimentation was observed.
- e. <u>Downstream Channel</u>. Bedrock is exposed for the entire width in the channel downstream of the dam. Some trees overhang the channel and some logs are lodged on an island in the center of the channel but otherwise the channel is generally wide and unobstructed. A bridge crosses the channel about 250 feet downstream of the dam. (See Appendix C Figure 11.) The channel downstream of this bridge is wide and unobstructed; mill buildings are located on the right bank of the channel. (See Appendix C Figure 12.) Further downstream, about 600 yards, is the water treatment plant. Beyond this, the river flows into the large pondage area of Salmon Falls River Dam, a low-head hydropower facility.

3.2 Evaluation

Based on the visual inspection, Rollinsford Dam is in fair condition.

Major seepage is discharging at three locations at the base of the dry stone-masonry training wall at the southwest end of the overflow section of the dam. Although this seepage has been mentioned in previous inspection reports dating back to 1940, insufficient information is available to conclude that it poses a potential problem.

Possible subsidence of the earth fill adjacent to the southwest end of the overflow section of the dam could adversely affect the stability of the southwest end of the dam.

Erosion of the ground between the northeast end of the dam and a nearby railroad bridge pier indicates that the northeast abutment has been overtopped. Future overtopping of the abutment could affect the stability of that abutment.

The dam has no usable low-level outlet to lower the pond in case of emergency.

SECTION 4 OPERATIONAL PROCEDURES

4.1 Procedures

No written operational procedures were found.

4.2 Maintenance of Dam

The Town of Rollinsford is responsible for the maintenance of the dam.

4.3 Maintenance of Operating Facilities

Since no operating facilities exist, this is not applicable.

4.4 Description of Any Warning System in Effect

No written warning system was revealed.

4.5 Evaluation

Maintenance procedures appear to be minimal. Leakages were observed that require attention and all operating facilities have been effectively discontinued by filling gates and openings with earth and gate operating mechanisms completely removed.

SECTION 5 HYDROLOGIC/HYDRAULIC

5.1 Evaluation of Features

- a. General. Rollinsford Dam is a run-of-the-river, split-stone and concrete gravity dam which impounds a reservoir of small size. At the southwest abutment there are remnants of an approach canal, gates, and penstock entrance structure. The approach canal and gate area have been filled with earth and the gate operators have been removed. The watershed above the dam consists of 230 square miles of gently to moderately sloping partly wooded terrain.
- b. Design Data. No original hydrologic and hydraulic design data were found.
- c. Experience Data. No information regarding past overtopping of Rollinsford Dam was revealed.
- d. <u>Visual Observation</u>. Based on the visual inspection it appears that overtopping may have occurred between the northeast spillway abutment and the railroad pier.
- Test Flood Analysis. Rollinsford Dam is classified as being rall in size having a hydraulic height of 20 feet and a maximum corage capacity of 820 acre-feet; the dam was determined to have a significant hazard classification because of potential damage to the railroad bridge and loss of the impoundment as a source of water to fight fires in Rollinsford. No loss of life is anticipated. Using the Recommended Guidelines for Safety Inspection of Dams, the test flood ranges from the 100-year to & the Probable Maximum Flood (PMF). Because the dam's size is in the upper range of the size classification, by PMF was selected as the test flood. The test flood inflow for Rollinsford Dam, having a drainage area of 230 square miles, was determined to be 34,500 cfs. Routing through the reservoir resulted in neglible surcharge storage effects in reducing peak inflows. Therefore, the routed test flood outflow is also equal to the inflow value of 34,500 cfs at elevation 82' NGVD. The test flood analysis indicates that the dam embankment would be overtopped by approximately 7.4 feet during test flood conditions (12 feet over the spillway). The maximum spillway capacity at top of dam is 7,010 cfs which is about 20 percent of the routed test flood outflow.
- f. Dam Failure Analysis. The impact of failure of the dam at top of dam was assessed using the Guidance for Estimating Downstream Dam Failure Hydrographs issued by the Corps of Engineers. The analysis covered the reach from the dam to Salmon Falls River Dam, a distance of 1 mile downstream. Salmon Falls River Dam, which is located 1 mile downstream of Rollinsford Dam, provides a large storage area for breach discharge. A breach would result in no loss of lives but may damage the piers of the railroad bridge and the Salmon Falls River Dam downstream. A breach discharge in the

reach between these two would stay in bank. Because the Rollinsford Dam is used for fire protection for the Town of Rollinsford, the loss of the pondage due to dam failure would be considered as public utility loss. The dam was classified Significant Hazard.

SECTION 6 STRUCTURAL STABILITY

6.1 Visual Observations

The visual examination indicates the following potential structural problems:

- a. Major seepage at the base of the dry stone-masonry training wall at the southwest end of the overflow section of the dam, which could adversely affect the stability of the gate structure and southwest end of the overflow section of the dam.
- b. Erosion of the ground between the northeast end of the overflow section of the dam and a bridge pier on the northeast abutment, which could adversely affect the stability of the northeast end of the dam and abutment.
- c. Possible subsidence of the earth fill next to the southwest end of the overflow section of the dam, which may be associated with piping that could adversely affect the stability of the dam.
- d. No usable low-level outlet to lower the pondage in case of emergency.

6.2 Design and Construction Data

No design and construction data are available.

6.3 Operating Records

None.

6.4 Post-Construction Changes

An inspection report of 8/10/70 indicates that the head gate channel has been filled in and effectively cuts off flow through the penstock. The penstock has been removed. The report of an inspection dated 11/30/77 indicates that the gate operators were removed and the penstock area filled with dirt.

6.5 Seismic Stability

This dam is located in Seismic Zone 2 and, in accordance with Phase I guidelines, does not warrant seismic analysis.

SECTION 7 ASSESSMENT, RECOMMENDATIONS, AND REMEDIAL MEASURES

7.1 Dam Assessment

- a. <u>Condition</u>. The visual examination indicates that Rollinsford Dam is in fair condition. The major concerns with respect to the integrity of the dam, if left uncorrected, are:
- (1) Major seepage at the base of the dry stone-masonry training wall at the southwest end of the overflow section of the dam.
- (2) Erosion at the northeast abutment, possibly the result of overtopping.
- (3) Possible subsidence of the earth fill next to the southwest end of the dam.
- (4) Uncertainty about the earth fill at the southwest abutment and consequent potential for erosion if area is overtopped.
- b. Adequacy of Information. The information available is such that the assessment of this dam must be based primarily on the results of the visual inspection.
- c. <u>Urgency</u>. The owner should implement the recommendations in 7.2 and 7.3 within one year after receipt of this Phase I report.
- d. Need for Additional Investigation. The information available from the visual inspection is adequate to identify the potential problems which are listed in 7.2 a below. These problems require the attention of a professional engineer experienced in the design and construction of dams who will have to make additional engineering studies to design or specify remedial measures to rectify the problems.

7.2 Recommendations

- a. The owner should engage a professional engineer qualified in the design and construction of dams to:
- (1) Re-establish a low-level outlet for the impoundment to use in case of emergency.
- (2) Inspect the downstream face of the concrete spillway when no water is flowing over the crest.

- (3) Investigate the seepage at the base of the dry stone-masonry training wall at the southwest end of the overflow section of the dam and design appropriate remedial measures.
- (4) Design repairs and erosion protection for the eroded area on the northeast abutment.
- (5) Design repairs for the subsided area of the earth fill at the southwest end of the overflow section of the dam.
- (6) Evaluate the earth fill at the southwest abutment with respect to erosion if overtopped, and to recommend remedial measures, if needed.

The owner should carry out the recommendations made by the engineer.

7.3 Remedial Measures

- a. Operating and Maintenance Procedures. The owner should:
- (1) Visually inspect the dam and appurtenant structures once a month.
- (2) Engage a professional engineer qualified in the design and construction of dams to make a comprehensive technical inspection once every year after the recommendations made in 7.2 a have been carried out.
- (3) Establish a surveillance program for use during and immediately after heavy rainfall and snowmelt and also a downstream warning program to follow in case of emergency conditions.
- 7.4 Alternatives. None.

APPENDIX A

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST PARTY ORGANIZATION

| PROJECT Rollinsford Dam, NH | DATE October 25, 1979 |
|---------------------------------------|---|
| | TIME 2:30 PM |
| | WEATHER Sunny, cool |
| D & DMV | W.S. ELEV. U.S. DN.S. 70 'NGVD55'NGVD |
| PARTY: 1. Warren Guinan (ANCO) | 6. Kenneth Stern (NHWRB) |
| 2. Stephen Gilman (ANCo) | 7. Ronald Hirschfeld (GEI) |
| 3. Leslie Williams (ANCo) | 8 |
| 4. Terri Sapp (ANCo) | 9 |
| 5. Mehdi Miremadi (ANCo) | 10 |
| PROJECT FEATURE Hydrology/Hydraulics | INSPECTED BY REMARKS M. Miremadi/ L. Williams |
| Structural Stability | S. Gilman |
| Soils & Geology | R. Hirschfeld |
| 4 | |
| 5 | |
| 6 | |
| 7 | |
| 8 | |
| 9 | |
| 10 | |

PERIODIC INSPECTION CHECKLIST PROJECT Rollinsford Dam, NH DATE Oct. 25, 1979 PROJECT FEATURE Intake Channel & Structure NAME DISCIPLINE ______NAME _____ AREA EVALUATED CONDITION OUTLET WORKS - INTAKE CHANNEL AND INTAKE STRUCTURE a. Approach Channel Slope Conditions Good Not visible beneath reservoir Bottom Conditions Rock Slides or Falls None Log Boom Debris Condition of Concrete Lining None Drains or Weep Holes Intake structures and gates are Intake Structure abandoned and filled in. Not operable and not visible for inspection. Condition of Concrete Stop Logs and Slots

PERIODIC INSPECTION CHECKLIST

| PROJECT Rollinsford Dam, NH | DATE Oct. 25, 1979 |
|--|---|
| PROJECT FEATURE Outlet Structure & | Channel NAME |
| DISCIPLINE | NAME |
| | |
| AREA EVALUATED | CONDITION |
| OUTLET WORKS - OUTLET STRUCTURE AND OUTLET CHANNEL | |
| General Condition of Concrete | No outlet works are visible. It appears that all outlet works at |
| Rust or Staining | the southwest abutment have been removed or filled in and abandoned |
| Spalling | removed or filled in and apandoned |
| Erosion or Cavitation | |
| Visible Reinforcing | |
| Any Seepage or Efflorescence | |
| Condition at Joints | |
| Drain holes | None observed |
| Channel | |
| Loose Rock or Trees Overhanging Channel | Some trees overhanging channel |
| Condition of Discharge Channel | Good. Some logs lodged on island at center of channel, but channel is generally wide and unobstructed |
| | |
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| | |

PERIODIC INSPECTION CHECKLIST PROJECT Rollinsford Dam, NH DATE Oct. 25, 1979 PROJECT FEATURE Spillway Weir NAME _____ _____ NAME _____ DISCIPLINE ____ CONDITION AREA EVALUATED OUTLET WORKS - SPILLWAY WEIR, APPROACH AND DISCHARGE CHANNELS a. Approach Channel Good General Condition None Loose Rock Overhanging Channel A few overhanging channel Trees Overhanging Channel Not visible beneath reservoir Floor of Approach Channel surface b. Weir and Training Walls Fair. Surface of concrete exposed General Condition of Concrete to water is eroded. Only at embedded item Rust or Staining -Several exposed areas are spalled Spalling to 1" depth. Coarse aggregate is exposed. Any Visible Reinforcing --Large quantity of water discharging Any Seepage or Efflorescence through stone masonry immediately downstream of southwest end of Drain Holes ___ spillway. None observed. c. Discharge Channel Good General Condition None Loose Rock Overhanging Channel Some Trees Overhanging Channel Bedrock Floor of Channel Some logs lodged on small island Other Obstructions at center of channel.

PROJECT Rollinsford Dam, NH PROJECT FEATURE Reservoir

DATE Oct. 25, 1979

| AREA EVALUATED | REMARKS |
|--|--|
| | |
| Stability of Shoreline | Good |
| Sedimentation | Not visible |
| Changes in Watershed Runoff Potential | None observed |
| Upstream Hazards | None |
| Downstream Hazards | Railroad bridge piers, road, da l mile downstream. |
| Alert Facilities | None posted |
| Hydrometeorological Gages | None |
| Operational & Maintenance Regulations | None posted. |
| | |
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APPENDIX B ENGINEERING DATA

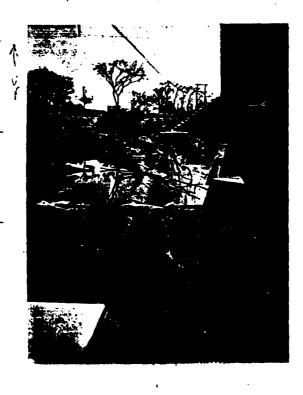
Mina To File

File

Sibject Inspection of Dan 205.02

Date 30 Mor 77

This dan is in good shape. The leakage mention by mr Rapoza & mr mare is still availant. The jute operators have been removed ord pentiock area. Filled with dint. There is a bot of debris on the spilling crest



MEMORANDUM

DATE: September 17, 1973

FROM: Donald M. Rapoza, Water Resources Engineer

SUBJECT: Dam inspection on Salmon Falls River in Rollinsford, N.H. - #205.02

TO: Vernon A. Knowlton, Chief Engineer, Water Resources Board

On September 10, 1973, I inspected the dam on the Salmon Falls River in Rollinsford. At the present time, the structure is owned by the Town of Rollinsford, which intends to convey the structure to the Salmon Falls River Watershed Association.

The structure is in fairly good shape: the left abutment (in Maine) has relatively little seepage. The right abutment has some leakage at the toe of the spillway. This leakage is not endangering the structure, but should be checked on a yearly basis for any increased discharge. The leakage has been reported in previous inspection reports. The concrete spillway is eroding and will have to be refaced sometime in the future.

I could not locate the leak in the spillway that Francis mentioned in his August 10, 1969 report. Perhaps debris had plugged the area in question.

DMR: js

State of New Hampshire WATER RESOURCES BOARD

EXMPOREMENTAL ST.

37 Green St.

Concord 08301

September 17, 1973

Mr. Wayne E. Murray Beamis and Davis 58 High Street Somersworth, NH 03878

Dear Mr. Murray:

This is in response to your letter requesting the New Hamp-shire Water Resources Board review the status of a dam owned by the Town of Rollinsford in the Salmon Falls River.

On September 10, 1973, I inspected the structure and found it to be in relatively good shape. There was some leakage at the right abutment which had been previously reported in other inspection reports. At this time there is no serious problems connected with this leakage, but the area should be inspected on a yearly basis.

Due to the flow over the spillway crest, I could not find the leak on the lip of the concrete spillway, as Mr. Moore mentioned in his August 10, 1969 report. There is the possibility that the area in question has been clogged with floating debris. To conduct a thorough inspection of the spillway, flow over the spillway would have to be bulkheaded, or the ponded area drawn down below the spillway crest.

The estimated costs of repairing the concrete lip in Mr. Moore's letter, dated March 3, 1972, should be increased by 20%, making a total of \$3.600.

Please feel free to call or write this office if you have any further questions.

Very truly yours,

Donald M. Rapoza Water Resources Engineer

DMR: js

DATE:

August 10, 1970

FROM:

Francis C. Moore, P.E. Water Resources Engineer

SUBJECT:

Salmons Falls Power Station Property - Rollinsford

TO:

Vernon A. Knowlton

Chief Water Resources Engineer

Forrest Hodgdon and I inspected Public Service Company of New Hampshire power station land and dam at Rollinsford, New Hampshire with Noel Sheldon on 8/6/70.

File

The land north of the power station is about 30 feet wide and about 350 feet from a town road, mainly occupied by a large pressure concrete penstock. This land would be useful to the mill, Sports Specialties Shoemaker Co. The balance of that lot except the power station and its immediate land would undoubtedly be retained for use of their Sub-Station.

The land across the river in Maine is steep for 50' to 75' from river and sloping to the old railroad right-of-way and highway line. It is remotely possible that the south end of this lot would possibly be of interest to Maine authorities if boat launching into the upper end of the Central Maine Power Company pool could be constructed. The land near the river is ledgy.

This dam is in fairly good shape. Some concreting of the spillway lip is needed to fill a serious leak about midway of the dam. The head gate channel has been filled in and effectively cuts off flow through the penstock to the power house. The shoe shop has an intake to a pipe line to a 75,000 gallon water tank on the hill to furnish fire protection to the mills. This intake is about thirty feet upstream of the gate house - a 5' concrete pipe set into the bank of the pond.

There is possible boat launching from the land at the New Hampshire end of the dam upstream of the intake canal. The river and pond could be navigated up to the next dam about 2 1/2 miles above. Some places the river is 1000' wide but averages around 200'.

The land in Maine at the end of the dam should be conveyed with the dam. It is less than one-third acre in size and offers no boat launching possibilities.

FCM/jb

NEW HAMPSHIRE WATER CONTROL COMMISSION

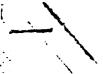
REPORT ON DAM INSPECTION

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| Other | ISOTWELLS . | AMM CE FIN | I STEMPLE | 41 There | 1.0 |
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NEW HAMPSHIRE WATER CONTROL COMMISSION

REPORT ON DAM INSPECTION

| TOWN | ROLLINSFORD | DAM NO. 205 | STREAMSal | mon Falls River | |
|-----------------------|-------------------------------------|------------------|------------|-------------------|--------------------------------|
| WMER | in State Gas & Ele | c.Co. ADDRESS _ | Dover N. F | | |
| | accordance with Senspected by me on | | | | bove |
| OTES ON I | PHYSICAL CONDITION | at shape | so abbo | ment Pral | <u>\(\sigma\) \(\sigma\)</u> |
| Spill | way for & 5 | with not | 0 | our pomz | - mait |
| Gates Amil 9 | main can | al gates in | good C | mation - | totral |
| nedto mian g II | | Ection and | | · futranc | <u>र्</u> |
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| EL'ARKS | Visite d p | men house o | priale | | |
| Con | y to Cwner D | Date | | | |
| , , o p, | , oo omer | B-6 | C D (| VSPECTOR VSPECTOR | - - |



NEW HAMPSHIRE WATER CONTROL COMMISSION DATA ON DAMS IN NEW HAMPSHIRE



| LOCATION | STATE NO. 205.U | |
|--------------------------------------|-------------------------------------|---------------------------------|
| | : County Strafford | |
| Stream Salmon Falls River | | |
| Basin-Primary Ocean | : Secondary Salmon Falls R. | |
| Local Nama | | |
| Coordinates—Lat. 43 15! - 4050 | : Long. 70°50° - 4000 | |
| GENERAL DATA | | |
| | i.: Uncontrolled Sq. Mi.: Total 230 | Sq. Mi. |
| Overall length of dam350ft.: Date of | of Construction | •••••••• |
| Height: Stream bed to highest elev15 | ft.: Max. Structure14!9" | ft. |
| | : Reservoir | |
| DESCRIPTION Gravity concrete sp | olitatone Foundation ledge | |
| Waste Gates | _ | |
| | | |
| Number: Size | ft. high x | ft. wide |
| Elevation Invert | : Total Area | sq. ft. |
| Hoist | | ******************************* |
| Waste Gates Conduit | | |
| | terials | |
| Sizeft.: Length | ft: Area | sq. ft. |
| Embankment | | |
| | | |
| | ft.: Min | |
| • | : Elev. | |
| | Downstream on on | |
| Length—Right of Spillway | : Left of Spillway | •••••• |
| Spillway | | |
| | concrete | |
| Length—Total255! | ft.: Net | ft. |
| Height of permanent section-Max | ft.: Min | ft. |
| Flashboards—Type Pin type. | : Height | ft. |
| | : Top of Flashboard | ************* |
| Flood Capacity 6885 c | fs.:cfs/sq. mi. | |
| Abutments | | |
| | | |
| | ft.: Min | ft. |
| Headworks to Power Devel (See "Data | | |
| OWNERP.SofNewHempshite | Menchester, N.H. | • |
| REMARKSCondition good Subject | et to inspection | |
| | • | |
| Use power | B-7 | |

NEW HAMPSHIRE WATER CONTROL COMMISSION DATA ON WATER POWER DEVELOPMENTS IN NEW HAMPSHIRE

| LOCATION | | | | AT DAM NO. 205.402 | |
|---|---|------------------------------|--|---|---------------------------------------|
| Town | llinsford | | CountyStra | fford | |
| Stream Sa | almon Falls R | • | | ····· | |
| Rasin-Primary | Ocean | | : Secondar | Salmon Falls H. | |
| | | | | *************************************** | |
| CENERAL DATA | \sim 200 \sim 2 | | | | |
| Head-May 45 | ft · Min | ft.: | Ave. | Public Utility | ft. |
| Data of Constru | ction | | Use of Power | Public Utility | |
| Date of Constitu | | ac ft · | Storage | e e e e e e e e e e e e e e e e e e e | ac ft |
| DESCRIPTION | *************************************** | | | Public Utility | e e e e e e e e e e e e e e e e e e e |
| | na katalan da | • • • • • | | and the second second second second second | · Septe. |
| Cine of Dook | Opening | | | | |
| Size of Par | Opening | •••••• | Matarial | | |
| Size of Dar | Phillips | 9a E4 | Nat | ी कार नहीं है के कार्युत्त करती. कारणाव क्षेत्रप्रवासकार कार्युत्त क्षेत्रहें के | |
| Area: Gross. Head Gates | | by. r | | | By. It. |
| Head Gates | | | | | |
| Type | | £L | | | d. |
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| Penstock | | | | • | |
| | | | | | |
| | | Length | *************************************** | | •••••• |
| Turbines | | | 2 Vanan | _ 9 | |
| | | | | | |
| Number | | : Makers | | n Smith | |
| Rating HP, no | er unit1500 | н.Р. са. : | Total Capacity | 3500 | нр. |
| Rating HP, no | er unit1500 | н.Р. са. : | Total Capacity | 3500 al | HP. cfs. |
| Rating HP. po Max. Dement Drive | er unit1590 C.F.S., per unit | H.P. ca. : | Total Capacity Tot | 3500 al | HP. |
| Rating HP. po Max. Dement Drive | er unit1590 C.F.S., per unit | H.P. ea. : | Total Capacity: Tot | 3500 al | HP. |
| Rating HP. po Max. Dement Drive Type | er unit1500 C.F.S., per unit | H.P. ca.: | Total Capacity: Tot | 3500 al | HP. |
| Rating HP. po Max. Dement Drive Type Generator | er unit1590 C.F.S., per unit | H.P. Ga. | Total Capacity: Tot | 3500 al | HP. |
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| Rating HP. po Max. Dement Drive Type Generator Number Make Rating KW | er unit1500 C.F.S., per unit 2 | H.P. ca. | Total Capacity: Total Capacity: Total Capacity | 3500 al ps = 600 v | HP. cfs. |
| Rating HP. po Max. Dement Drive Type Generator Number Make Rating KW | er unit1500 C.F.S., per unit 2 | H.P. ca. | Total Capacity: Total Capacity: Total Capacity | 3500 al ps = 600 v | HP. cfs. |
| Rating HP. po Max. Dement Drive Type Generator Number Make Rating KW., Exciter Number | er unit1500 C.F.S., per unit 2 Westinghous per unit | H.P. ca. : | Total Capacity: Total Capacity: Total Capacity | 3500 al ps 600 v 1000 | HP. cfs. |
| Rating HP. po Max. Dement Drive Type Generator Number Make Rating KW., Exciter Number | er unit1500 C.F.S., per unit 2 | H.P. ca. : | Total Capacity: Total Capacity: Total Capacity | 3500 al ps 600 v 1000 | HP. cfs. |
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| Rating HP. po Max. Dement Drive Type | er unit | e1250.k.: : Make | Total Capacity: Total Capacity | 3500 al ps = 600 v 1000 | K. W. |
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| Rating HP. po Max. Dement Drive Type | er unit | H.P. 68. : | Total Capacity: Total Capacity | 3500 al ps - 600 v 1000 | K. W. |

PUBLIC SERVICE COMMISSION OF NEW HAMPSHIRE-DAM RECORD

I-4897

| TOWN | Rollinsford | TOWN 2 | NO. 205 02 |
|------------------------------------|---------------------------------|--------------------------------------|--------------------|
| RIVER STREAM | Salmon Falls River | | |
| DRAINAGE AREA | | POND AREA | |
| DAM TYPE | Gravity | FOUNDATION Ledge | |
| MATERIALS OF | Concrete, Split Stone | | |
| PURPOSE OF DAM | POWER-CONSERVATION-DOMESTIC-REC | REATION-TRANSPORTATION-PUBLIC | UTILITY |
| HEIGHTS, TOP | OF STREAM 19' ADDIOX. | TOP OF DAM TO SPILLWAY CRESTS | |
| SPILLWAYS, L | engths Approx. 255† | | OF DAM ADDROX. 350 |
| FLASHBOARDS | 3 * ±11 | | |
| OPERATING HE | EAD 451 | TOP OF FLASHBOARDS TO N. T. W. | |
| WHEELS, NUM | z-morgan builth 1500 Hr | each | |
| GENERATORS, KINDS & K. W | NUMBER | | |
| H. P. 90 P. C. 1 100 P. C. EFF. | TIME | H. P. 75 P.C. TIME 100 P. C. EFF. | |
| REFERENCES, PLANS, INSPEC | | | |
| | | | ₹ |

OWNER - Public Service Co. of N. H.

CONDITION - Good

MENACE - Yes. Will be subject to periodic inspection.

To the Public Service Commission:

The foregoing memorandum on the above dam is submitted covering inspection made November 6, 1935, according to notification to owner dated November 4, 1935, and bill for same is enclosed.

Nov. 14, 1935 Copy to Owner Samuel J. Lord Hyd. Eng.

NEW HAMPSHIRE WATER RESOURCES BOARD

INVENTORY OF DAMS AND WATER POWER DEVELOPMENTS

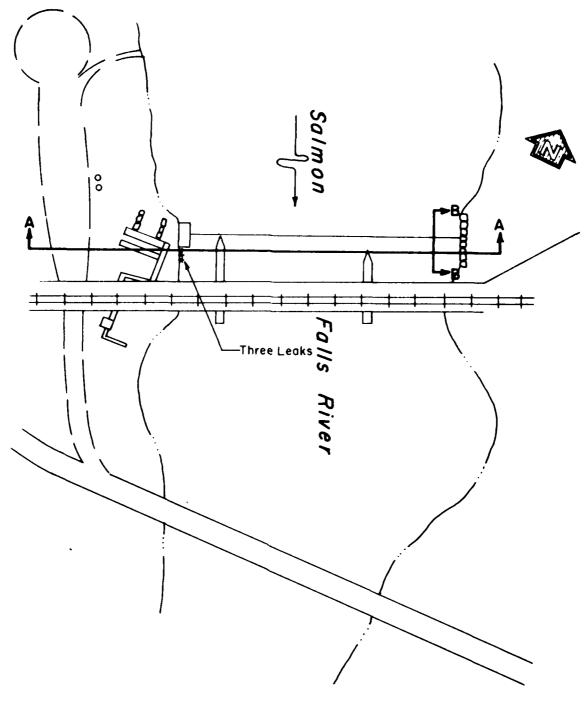
| RIVER | Ocean | | NO. | 2 - | 12 - | I-4897 | |
|------------|-------------------------|--------------------|---------------------------|---|---------------------|-------------------------------------|-----------|
| | Salmon | Falls | | | | I-4897 | |
| TOWN | Rolli. | usforo | OWNE | R Public Serv | ICE Ca. O | INH. Man | checter |
| LOCAL NAM | | | · | | | | |
| BUILD | | DESCRIP | Ledge | VIEY C | oncrete | Split Stan | <u>e</u> |
| | | | <i>-</i> | | | | |
| POND AREA | | तेस उक्तर | DRAMDOMM 1 DAM-FO. 192 | | | ACITY-ACRE | FT • |
| OVERALL LI | ENGTH OF | DAM-FU. | 750 = HAX | FLOOD HELD | | E CREST-FT. | |
| PERMANENT | CREST EL | EV.U.S. | 4.5. | | L GAGE | | |
| PAILWATER | | EV.U.S. | | | L GAJE | | |
| SPILLWAY 1 | LENGTHS -F | T. 24 | ~~ / | FREE | BOARD-FT | | |
| FLASHEOARI | ds-Type, : | HEIGHT | ABOVE CREST | 1.25 F | | | |
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| REMARKS | Conditi. | ou for | d | Free bear | YFEE | C. CAUID NE | 117 |
| & L wto A | SCATABU | OR. ATT | outic Ocean fi | Vu 14508 | c fors | SKEFELL | |
| | • | | | | | | |
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| SalmonFoll | S Station | PS Cou | | | | | |
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| JNITS NO. | ELOPMENT RATED HP | HEAD FEET AS | C.F.S. FULL GATE | /000 €2 | West/ 1205 | rowseith | (12.O.KV) |
| JSE_ | ELOPMENT RATED HP | HEAD FEET AS | C.F.S. FULL GATE | /000 €2 | West/ 1205 | en South inghouse 6 A 225 APM | (12.O.KV) |
| | ELOPMENT RATED HP | HEAD FEET AS | C.F.S. FULL GATE | /000 €2 | West/ 1205 | en South inghouse 6 A 225 APM | (12.50.KV |
| INITS NO. | ELOPMENT RATED HP | HEAD FEET AS | C.F.S. FULL GATE | /000 €2 | West/ 1205 | en South inghouse 6 A 225 APM | (12.O.KV) |

B-10

DAGE 11/6/30

CALCULATION SHEET Made By Mestinghous 1000KW 1250KVN

CRAINAGE AREA NAME OF COMPANY Balmon Falls rown Rollingroce, N. H. Mo. 165 Talmon Falle Mfg. Co. Balmon Falle, N. H. RATE BEC. FT. PER SQ. MI. BO% TIME RESOURCES HE~D FOR ISOLATED INDUSTRIAL PLANTS FOR ISOLATED INDUSTRIAL PLANTS __ 3000 48 pt PAGE NO. 10 1077.00



Anderson-Nichols & Co., Inc

CONCORD

NEW HAMPSHIRE

ON ARMY ENGINEER DIV NEW ENGLAND
CORPS OF ENGINEERS
WALTHAM, MA.

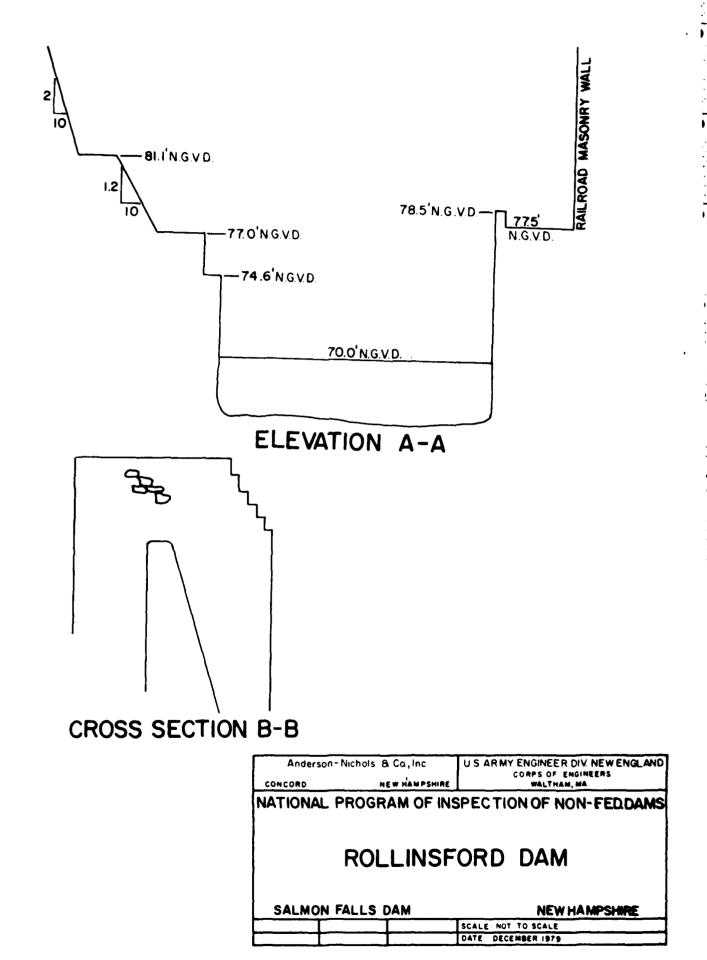
NATIONAL PROGRAM OF INSPECTION OF NON-FED. DAMS

ROLLINSFORD

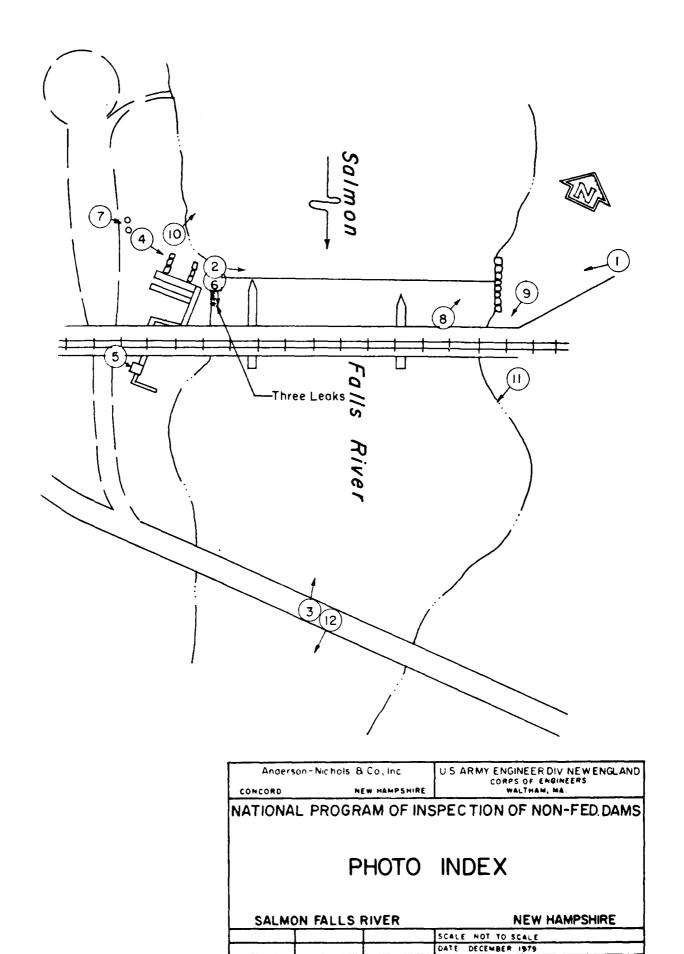
SALMON FALLS RIVER

SCALE NOT TO SCALE

DATE. DECEMBER 1979

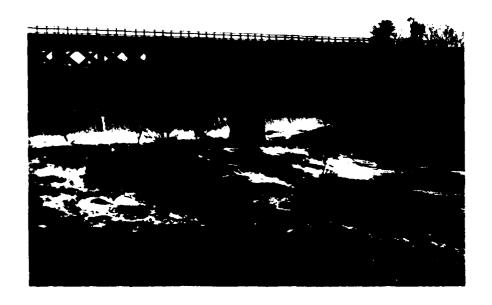


APPENDIX C
PHOTOGRAPHS





October 25, 1979
Figure 2 - Looking northeast across spillway crest.



October 25, 1979
Figure 3 - View of the downstream face of the dam
from the road crossing just downstream.



October 25, 1979
Figure 4 - View of the filled in approach channel and gate structures.



October 25, 1979
Figure 5 - Looking at an inoperable gate on the southwest end of the dam.



October 25, 1979
Figure 6 - View of the three leakages at the southwest end of the spillway.



October 25, 1979
Figure 7 - Looking at the two pipes which are utilized to obtain water from the impoundment for use in fire protection for Town of Rollinsford.



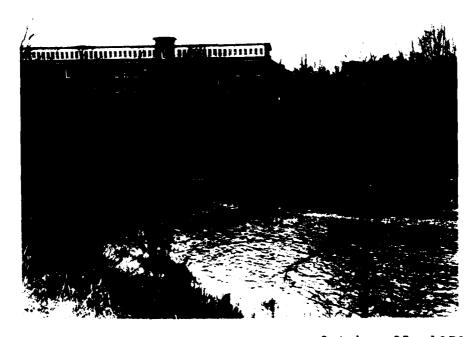
October 25, 1979
Figure 8 - View of the northeast spillway abutment.



October 25, 1979
Figure 9 - Looking at erosion between the northeast spillway abutment and railroad pier.



October 25, 1979
Figure 10 - Looking upstream into the reservoir from the southwest abutment.

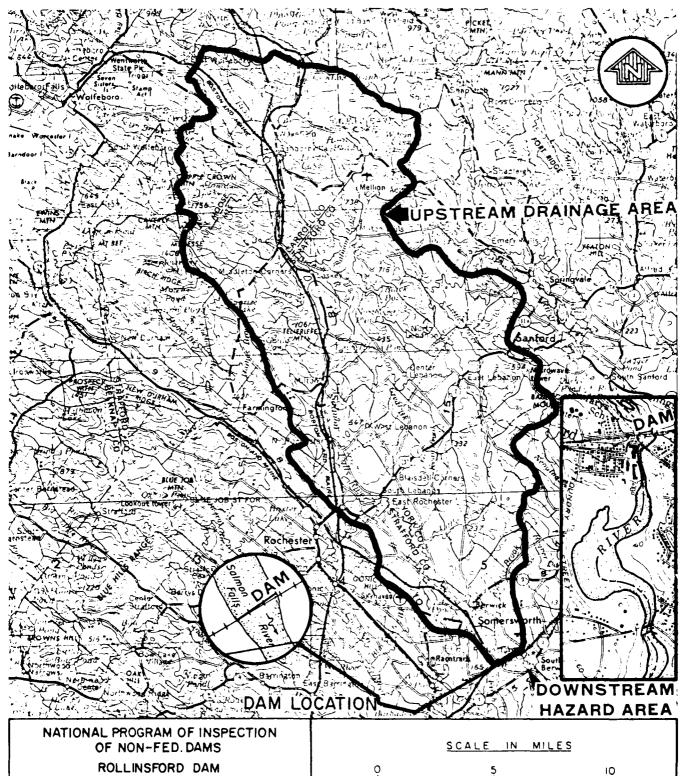


October 25, 1979
Figure 11 - Looking downstream at the road crossing from the northeast discharge channel.



October 25, 1979
Figure 12 - View of the channel downstream of the road crossing shown on Figure 11.

APPENDIX D
HYDROLOGIC AND HYDRAULIC COMPUTATIONS



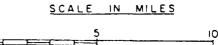
ROLLINSFORD, NEW HAMPSHIRE REGIONAL VICINITY

DECEMBER 1979

DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION, CORPS OF ENGINEERS WALTHAM, MASSACHUSETTS

ANDERSON-NICHOLS & CO,ING

CONCORD, NH



MAP BASED ON U.S.G.S. I: 250,000 SERIES TOPOGRAPHIC MAPPING. NK 19-1 PORTLAND ME.-N.H. 1956.

Masumptions:

ruspose: Destinance degree of the bysasa.

1- No plant cond.

2- Breach occure at lands dam

Following equation is used for perk outflow

QP, = 3 No V8

where Wb = kireach and the 100 Ft tailwater select = 51.8 Ho = 76.8 - 57.8 = 14.0 rt

TOTA Breach & = 13925

DAM LOCATED DIS OF KULLINSFORD DAM:

D. A. = 232 Mi length of the daw = 362 length of spelling=250 Ft

WEIR SECTION DATA:

| STATION | 1 LEVATION |
|---------|------------|
| 0 | 27.5 MsL |
| 60 | 27.5 |
| 60 | 20' |
| 278 | 20' |
| 278 | 27.5 |
| 362 | 27.5 |

A SOUTH THE THE PARTY OF CURTE (FOR DAM WS)

A SOUTH FATTE OF CLASED.

STAGE (FT MSL)

DISCHARGE SES

20

25 Q = 2.9(218)(5) = 7070

 $27.5 \qquad \mathcal{L} = 2.7 \left(218\right) \left(7.5\right)^{3/2} = 13000$

30 $\chi = 2.9(84)(2.5) + 2.9(218)(10) + 2.9(60)(2.5)^{3/2}$

= 765 + 20001 + 688

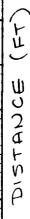
= 21650 CF5

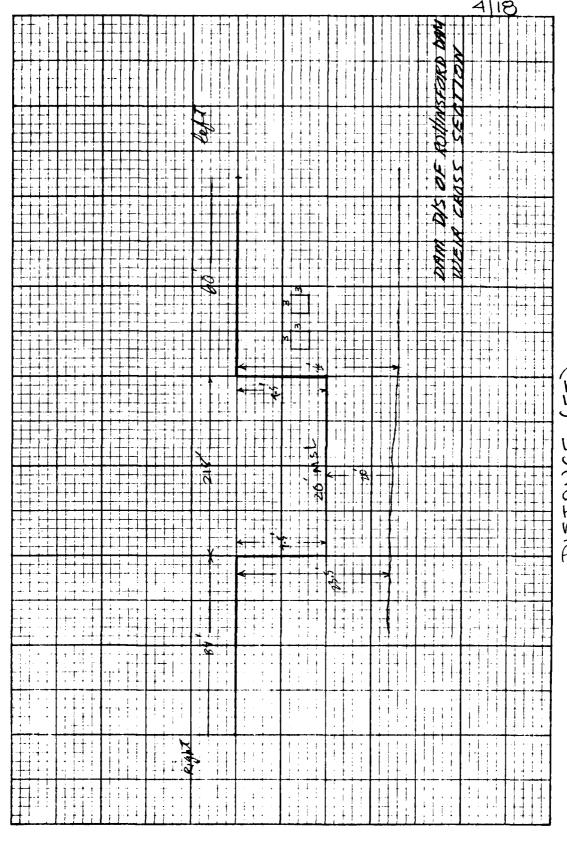
REFER TO RATING CURVE (P.5)

AT 13925 CKS (BREACH Q) = FLEV. = 27.8 MSL

ELEV. TOP OF LAW = 27.5 MSL

THE DAM WILL OVER SPILLING CREST = 7.8'





1

COOL MAN

NORMAL POOL 1. LEVATION = 20 MSL

SURFACE AREA AT NORMAL POOL = 40 ACRES

ASSUME CHANNEL DEPTH = 10'

NORMAL POOL STORAGE = 400 AC-FT

USING FRUSTRUM OF PYRAMID EQUATION

V = V3 h (b1 + b2 + \(\bar{b}_1 \bar{b}_2 \))

WHERE h= E/EV. ABOVE NORMA/ POO! (ET)
b, = NORMA! POO! SURFACE AREA(AC)
br = ENLARGED SURFACE AREA(AC)

40 4130 AC-FJ

40 AC-FJ

20' A00 AC-FJ

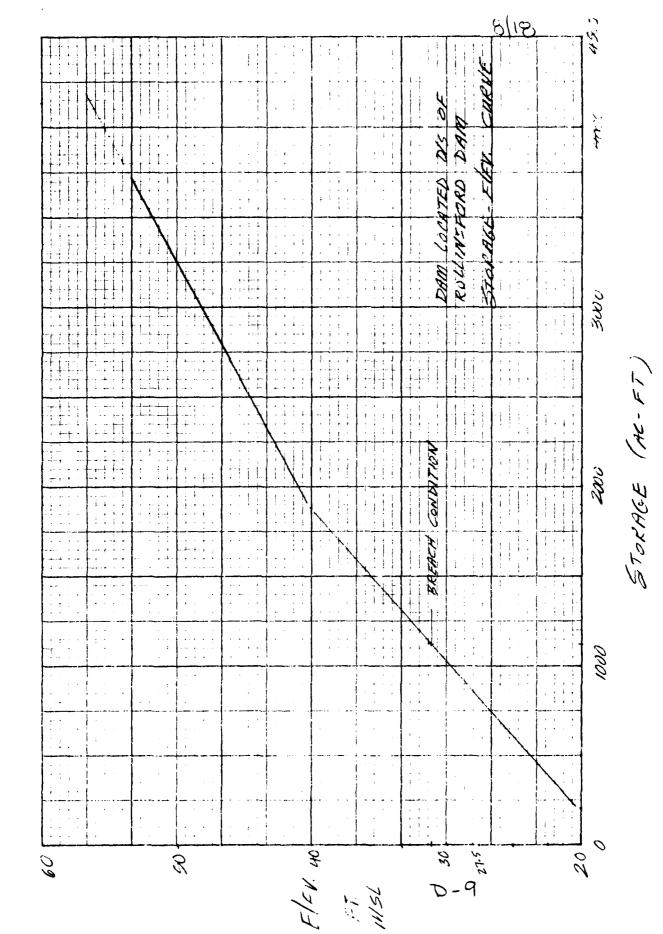
7/18

AT E/EV. 27.8 NISL (BRENCH & E/EV.)

STORMGE = 1125

NORMAL STORMGE = 400

SURCHARGE STORME = 1/25-400 =



Anderson-Nichols & Company, Inc.

Subject RollINSFULD DAM

Sheet No. 9 of 18
Date 1/-30 - 79
Computed MNM

JOB NO.

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 1/4 IN. SCALE

DIS HAZAKD ANALYSIS:

H RAILRUAD ERIDGE IS LOCATED JUST DE OF THE DAM. THE BRENCH DISCHARGE MIGHT DAMAGE THE PIERS OF THE RAILROAD BRIDGE.

AN ACTIVE MILL BUILDING IS LOCATED ABOUT 300' DIS OF THE DAIN, AND IS PROTECTED BY A CONCRETE TRHINING WALL

AN ABANDUNED MILL BUILDING IS LOCATED ABOUT 500' DIS OF THE DAIN WHICH WOULD BE EFFECTED BY BREACH DISCHARGE.

SALMON FAILS RIVER DAIN WHICH IS LOCATED ABOUT
I WHILE DIS OF KULLINSFORD DAIN PROVIDES
A LARGE STURMGE HREA FOR BREACH
DISCHARGE, RESULTING IN ATTENUATION
OF THE BREACH WHIE. ROLLINSFORD DAIN,
BREACH COULD OVER TOP THIS DAIN BY 0.3
OF WATER.

ROLLINSFORD DANN IS A FUBLIC UTILITY DAM (USED FOR FIRE PRITECTION FOR THE TOWN OF ROLLINSFORD), THEREFORE THE LOSS OF PONDAGE DUE TO DAIN FAILURE WOULD BE CONSIDERED A PUBLIC UTILITY LOSS. ROLLINSFORD WAS TREISFORD CLASSIFIED -

D-10

Anderson-Nichols & Company, Inc.

Subject MOLL

Subject KOLLINSFORD DAM

Sheet No. 10 of 18
Date 11-27-79
Computed 14 11 14

JOB NO.

DRHINAGE AREA = 230 INI 2

SIZE CLASSIFICATION = SMALL

HAZARD CLASSIFICATION = SIGNIFICANT

TEST Flood = ½ PMF

CALCULATE PMF USING "PRELIMINARY GUIDANCE FOR

ESTIMATING ILLAXIMUM PROBABLE DISCHARGES IN

PHASE I DAM SAFETY INSPECTION, MARCH, 1978"

USING FLAT & COASTAL (NEVE TO DETERMINE PINE

PMF = 300 CFS

WITH 2300 CFS

PEAK INFLOW = ½ PMF = ½ 67000 = 34500 CFS

D-11

Anderson-Nichols & Company, Inc.

Subject KOLLINSFORD DHIVI

Sheet No. 11 of 18

Date //- 27-79

Computed AJA/JJJ

Checked

JOB NO.

37 38

SQUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29

DETERMINING RATING CILRVE USE WEIR EQUATION Q = C L H 3/2 WHERE * C = 2.9 FER CONCRETE SECTION 8 C = 2.6 FOR WOODED EMBANKMENT 10 11 12 DISCHARGE STAGE (FT) 13 (CFS)14 70 15 3/2 16 x = 2.1(245)(2) = 201072 17 18 x= 1.9(245)(4.6) = 1010 74.6 19 $\omega = 29(245)(6)^{3/2} + (2.9)(15)(1.4)^{5/2} = 10515$ 20 76 21 3/2 = 2.9(245)(1) + (2.9)(15)(2.4) = 1332022 77 23 Q = 2.9(245)(7.5) + 2.9(15)(2.4) + 2.6(50)(0.5)24 77.5 25 + 1/2(2.6)(4.2 (0.5)3/2 14595 + 215 + 50+2 26 = 14860 27 Q = 2.6(71)(1) + 2.1(245)(8.5) + 2.9(15)(3.9) +28 78.5 29 Z.6(00X1.5)312 4 (1.6)(12.5)(1.5)-185+17610+335 30 + 239 + 30 = 18400 31 32 33 * "C" VALUES WERE THEEN FROM BRATIR & KING HANDBOOK 34 OF HYDRAUKICS' 21-5 36

Sheet No. 17 of 18

Date 1/- 27 - 79

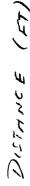
Computed 1/1/1/1

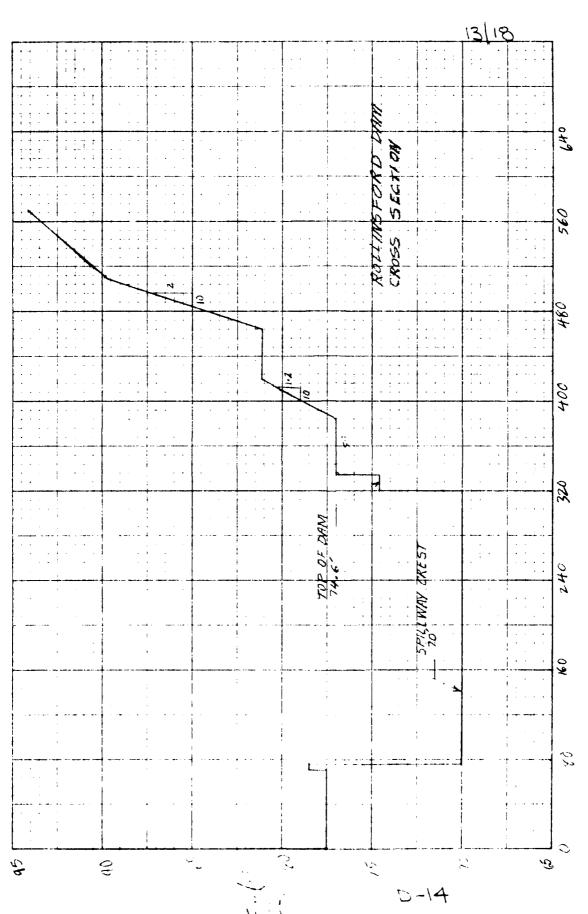
Checked

JOB NO.

33

STAGE (FT) DISCHARGE Q = 2.6(71)(3.6) + 2.9(4)(2.6) + 2.9(245)(11.1) 81.1 + 2.9 (15)(6.5) 312 + 2.6(50)(4.1) 32 1/2 (2.6)(34)(4.1) = 1261 + 49 + 26275 + 721 + 1080 + 367- 29750 Q = 2.6(71)(4.5) + 2.9(4)(3.5) + 2.9(245)(12)82 +2.9(15)(7.4) 3/2 + 2.6(50)(5) 3/2 + /2 (2.6)(42)(5) 3/2 12 +2.6 (45)(0.9) 32+1/2 (2.6)(4.5)(0.9) 32 13 = 1762 + 76 + 29535 + 876 + 1453 + 610 +100+5 = 3450015 16 17 TOTAL TEST FLOOD INFLOW = 34500 CFS 18 REFER TO CURVE ON PAGE 19 AT 34500 CFS => E/EV. = 82 MSL 20 21 THE DEPTH OF WATER OVER SPILLWAY CREST 22 DURING KIPMF WILL APPROXIMATELY BE 24 82' - 70 = 12'25 THE DAM WILL BE OVERTOPPED BY 26 82'-74.6'= 7.4' 27 28 29 DURING V2 PMF 30 31 32





Anderson-Nichols & Company, Inc.

Subject RollINSFORD DAM

Sheet No. 4 of 8
Date 11-27-79
Computed 44NA4
Checked

JOB NO.

SUUARES 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30

2

10

12

13

15 16

24

25

27

28

31

35

38

SURFACE AREA AT NORMAL POUL = 57 ac ASSUME a diplose & F.t. NORMAL POUL STORAGE = 456 ac-FT.

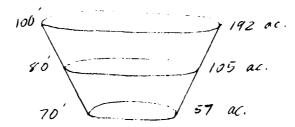
USE FRUSTRUM OF PYRAMID EQUATION

WHERE

h = Elev. ABOVE NORMH! POOL (FT)

bi = NORMH! POOL SURFACE AREA (ac)

bi = ENLARGED SURFACE AREA (AC)



AT Elev. 80 MSL = * SURFACE AREA = 105 ac

TOTAL STORAGE = 456+800 = 1256 AC. AT AT Elev. 100' MSC => SURKACT AREA = 192 AC.

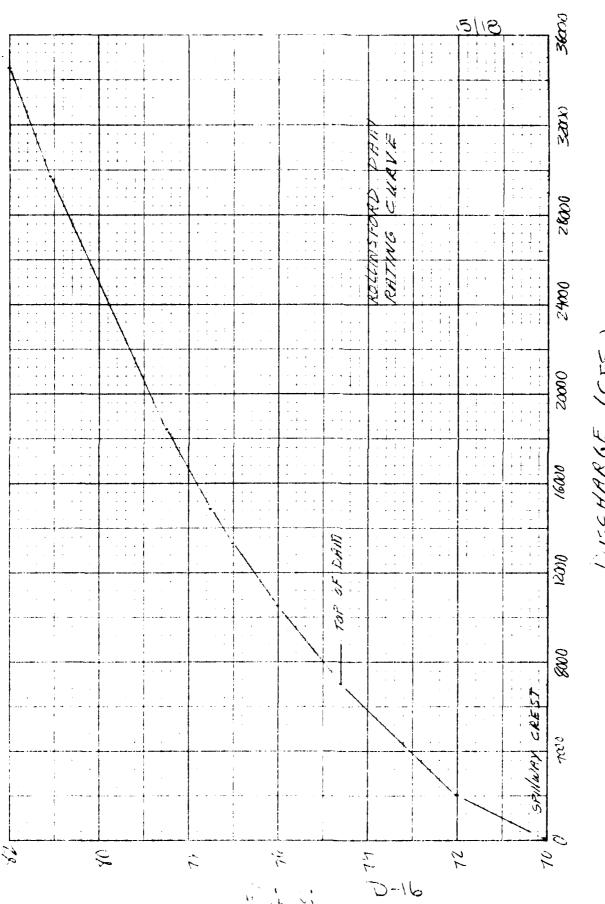
$$V = V_3(20)(105 + 192 + \sqrt{105})(192) = 2635 \text{ ac-FT}$$

TOTAL STOKAGE = 2635 + 1256 = 3891 ac-FT

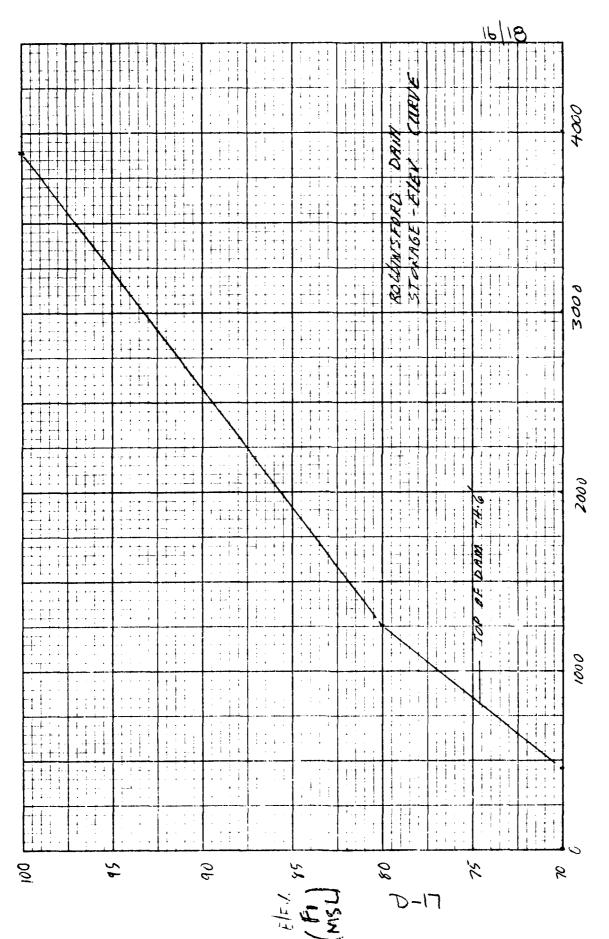
* SURFACE AREAS WERE PLANIMETERED OFF 11565 WHAD SHEETS.

7-15

DISCHARGE (CFS



STORAGE (QC-FT)



Anderson-Nichols & Company, Inc.

JOB NO.

1.3

. 16

17

20

20

130

31

QUAPES 0 1 2 **3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30**

DETERMINE SUNCHINGE HIGHT TO FASS OF, OF 34390 (PS.

| Ande: | rson-Nichols & Company, Inc. | Sheet No. 18 of 18 Date |
|------------------|--|-------------------------|
| | JOB NO. | Checked |
| IUARES IN. S. | © 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 | 21 22 23 24 25 26 27 |
| | 2 3 AT ELEV. 81.9 MSL => WISCHARGE | = 34200 CFS |
| | 4 | |
| | 6 NORAINE STORMEL = 1136 | NC-FT |
| • | NAXIMAM STURNER = 820 A | と- ドブ |
| | storage effects of down will be negligible. |)-e |
| • | Test Flood discharge - 34,500 cts Test Flood elevation - 82' MSL | د |
| ĭ | 15 Dan will be overtoped by 7.4 16 (12 feet over spillway crest) do 17 test flood of 12 PMF. | reet |

 70-19

APPENDIX E

INFORMATION AS CONTAINED IN THE NATIONAL INVENTORY OF DAMS NOT AVAILABLE AT THIS TIME

FILMED

8-85

DTIC